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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aide in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general

condition and the downstream damage potential.

Accessionior NTIS GNALL DDC TAB Unannounced Justification

SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered) The total discharge capacity of the spillways is adequate to impound and safely discharge the floodwaters resulting from the Probable Maximum Flood (PMF). Several minor deficiencies were noted on this structure. Among these deficiencies were a small depression on the upstream slope near the riser, ponding of water in the bottom of the auxiliary spillway channel, and a substantial accumulation of debris around the intake of the principal spillway riser. These deficiencies should be corrected within 6 months of the date of notification of the owner. In addition, an emergency action plan for notification of downstream residents should be developed within 6 months.

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered) READ INSTRUCTIONS REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM 1. REPORT NUMBER 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER 9D-A084 57 4. TITLE (and Subtille)
Phase 1 Inspection Report 5. TYPE OF REPORT & PERIOD COVERED Phase I Inspection Report Finch Hollow Watershead Project - Site 2 National Dam Safety Program Susquehanna River Basin, Broome County, NY 6. PERFORMING ORG. REPORT NUMBER Inventory No. NY 719 7. AUTHOR(a) 8. CONTRACT OR GRANT NUMBER(e) George Koch, P.E. DACW-51-79-C-0001 9. PERFORMING ORGANIZATION NAME AND ADDRESS 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS New York State Department of Environmental Conservation/50 Wolf Road Albany, NY 12233 11. CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE 30 May 1980 New York State Department of Environmental Con-13. NUMBER OF PAGES servation/ 50 Wolf Road Albany, New York 12233
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18. SUPPLEMENTARY NOTES

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Dam Safety National Dam Safety Program Visual Inspection Hydrology, Structural Stability

Finch Hollow Watershed Project Site 2 Broome County Dickinson

20 ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization.

The examination of documents and visual inspection of the Finch Hollow of Site 2 Dam did not reveal conditions which constitute a hazard to human life or property. y wer

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UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

PHASE T-INSPECTION REPORT

MATIONAL DAM SAFETY PROGRAM

FINCH HOLLOW WATERSHED PROJECT SITE 2 (Toventory Number 719)

SUSQUEHANNA RIVER BASIN

BROOME COUNTY, NEW YORK

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PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

Name of Dam:

Finch Hollow, Little Choconut &

Trout Brook Watershed Project

Site 2 I.D. No. NY 719

State Located:

New York

County Located:

Broome

Watershed:

Susquehanna

Stream:

Little Choconut Creek

Date of Inspection:

November 8, 1979

ASSESSMENT

The examination of documents and visual inspection of the Finch Hollow Site 2 Dam did not reveal conditions which constitute a hazard to human life or property.

The total discharge capacity of the spillways is adequate to impound and safely discharge the floodwaters resulting from the Probable Maximum Flood (PMF).

Several minor deficiencies were noted on this structure. Among these deficiencies were a small depression on the upstream slope near the riser, ponding of water in the bottom of the auxiliary spillway channel, and a substantial accumulation of debris around the intake of the principal spillway riser. These deficiencies should be corrected within 6 months of the date of notification of the owner. In addition, an emergency action plan for notification of downstream residents should be developed within 6 months.

George Koch

Chief, Dam Safety Section New York State Department

of Environmental Conservation

Devora Koch

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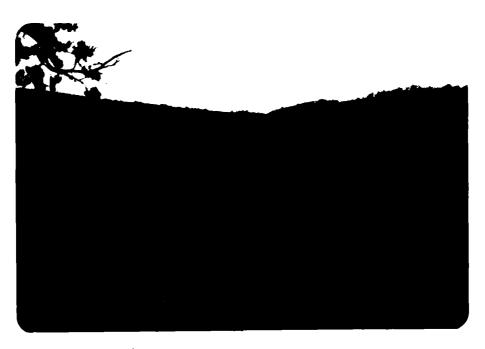
Approved By:

Col. Clark H. Benn

New York District Engineer

Date:

30 my 80



OVERVIEW - UPSTREAM FACE FINCH HOLLOW WATERSHED PROJECT SITE 2 I.D. No. NY 719



OVERVIEW - DOWNSTREAM FACE

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
FINCH HOLLOW, LITTLE CHOCONUT, & TROUT BROOK WATERSHED PROJECT
SITE 2
I.D. No. NY 719
(#96A-3844)
SUSQUEHANNA RIVER BASIN
BROOME COUNTY, NEW YORK

SECTION 1: PROJECT INFORMATION

1.1 GENERAL

a. Authority
The Phase I inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367.

b. Purpose of Inspection
This inspection was conducted to evaluate the existing conditions of
the dam, to identify deficiencies and hazardous conditions, to determine
if these deficiencies constitute hazards to life and property, and to
recommend remedial measures where required.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam
The Finch Hollow Watershed Project Site 2 consists of an earth dam with a service spillway conduit passing through the embankment and an auxiliary spillway passing around the eastern end of the embankment.

The dam consists of a zoned compacted earth embankment which is 57 feet high, has a crest length of 1050 feet and a crest width of 14 feet. The upstream slope is 1 vertical on 3 horizontal and the downstream slope is 1 vertical on 2.5 horizontal. The crest and exposed slopes are covered by crownvetch. An earth cutoff trench of varying depth and width keys the embankment into the foundation soils.

The principal spillway consists of a rectangular concrete drop inlet structure, a rectangular cast-in-place concrete conduit 6 feet wide by 7 feet high, and a plunge pool cut into bedrock at the outlet end of the conduit. A reservoir drain consisting of a 24 inch diameter cast-iron pipe extends from a point out in the reservoir to the base of the principal spillway riser, a vertical slide gate mechanism mounted along the inside of the riser controls the flow through the reservoir drain. The auxiliary spillway is in a rock cut and has a bottom width of 75 feet.

An internal drainage system consisting of a gravel and sand filter with perforated 10 inch diameter asbestos cement collector pipes is located at the base of the embankment near the downstream toe. Seepage is collected and conducted through this drain and outleted into the plunge pool.

b. Location Finch Hollow Watershed Project Site 2 is located on the Little Choconut Creek, approximately 3/4 miles north of Johnson City. A four lane highway going to the county airport is adjacent to the reservoir. The dam is in the Town of Dickinson, New York.

c. Size Classification
The dam is 57 feet high and has a maximum storage capacity of 1480 acre-feet. Therefore, the dam is in the intermediate size category as defined by the Recommended Guidelines for Safety Inspection of Dams.

d. Hazard Classification
The dam is classified as "high" hazard due to the presence of a number of homes in Johnson City and a major highway downstream of the dam.

e. Ownership
The dam is owned and operated by the County of Broome, New York. The contracting office's representative is Charles Kark. His phone number is (607)772-2114.

f. Purpose of Dam
The dam is a floodwater retarding structure.

g. Design and Construction History
The dam was designed by the U.S. Department of Agriculture, Soil Conservation
Service (SCS). The dam was constructed in 1972 by the Port Cannon Construction
Company of Vestal, New York. The SCS office at the Broome County Airport has
a design folder containing hydrologic, hydraulic and structural design
information, in addition to the as-built plans and contract documents.

h. Normal Operating Procedures
Normal flows are discharged through the principal spillway. This structure
has sufficient capacity to store and discharge a 100 year flood without
discharge occuring in the auxiliary spillway. For storms in excess of the
100 year flood, discharge through the auxiliary spillway can be expected.

1.3 PERTINENT DATA

a. Drainage Area(sq. mi.)	11.72
b. Discharge at Dam (cfs) Principal spillway at maximum high water	1,493
Principal spillway at auxiliary spillway crest elevation Auxiliary spillway at maximum high water	1,092 31,403
Reservoir drain at principal spillway crest elevation	48
c. Elevation (USGS Datum)	976.4
Top of Dam Auxiliary Spillway Crest	950.8
Principal Spillway Crest Reservoir Drain, invert elevation	931.6 922.9

<u>d.</u>	Reservoir Surface Area (acres)	
	Top of Dam	69.0
	Auxiliary Spillway Crest	30.9
	Principal Spillway Crest	4.7
<u>e.</u>	Storage Capacity (acre-feet)	
	Top of dam	1480
	Auxiliary Spillway Crest	300
	Principal Spillway Crest	20

f. Dam Embankment type - A 3 zoned compacted earth fill with a keyed earth cut-off trench and drain parallel to axis of dam

Embankment length(ft)	1050
Slopes Upstream	l vertical on 3 horizontal
Downstream	1 vertical on 2 1/2 horizontal
Crest width(ft)	14

Weir length (ft) 32.0

h. Auxiliary Spillway	
Type: Channel cut into bedrock with trapezoidal	cross section
Bottom Width(ft)	75
Side Slopes (V:H)	1:3
Length of level section(ft)	50
Exit Slope(ft/ft)	0.019

i. Reservoir Drain
Type: 24 inch diameter cast iron pipe with reinforced concrete inlet
Control: Manually operated vertical slide gate mounted along the inside of the principal spillway riser.

SECTION 2: ENGINEERING DATA

2.1 GEOTECHNICAL DATA

a. Geology

The Finch Hollow Watershed Project Site 2 Dam is located in the glaciated portion of the Appalachian uplands (northern extreme of the Appalachian Plateau) physiographic province of New York State. These uplands were formed by dissection of the uplifted but flat lying sandstones and shales of the Middle and Upper Devonian Catskill Delta. The plateau surface is represented by flat-topped divide with drainage generally southwest toward the Susquehanna River system.

Glacial cover is generally thin, although some north-south valleys are so thick that they are completely buried. The present surficial deposits have resulted primarily from glaciations during the Cenozoic Era, the last of which was the Wisconsin glaciation, approximately 11,000 years ago.

b. Subsurface Investigations

A subsurface investigation program was conducted by SCS in 1966 prior to construction of the dam. This program consisted of 37 drill holes and 32 test pits at locations along the dam, auxiliary spillway, structural elements, and borrow area. Applicable subsurface information is included in Appendix E (Drawings #25 and 26.)

In general, the soils in the vicinity of the dam are of glacial till origin, gravelly silts and silts overlying a shaly silt - stone bedrock from 10 to 30 feet below the original ground surface. With the exception of those soils having high gravel contents, the soils are of low or very low permeability.

2.2 DESIGN RECORDS

The dam was designed by the Soil Conservation Service, who prepared a design report. A folder containing the design report and other design information was available at the SCS office at the Broome County Airport. Twenty-six drawings, several of which have been included in Appendix E, were prepared for the construction of this dam.

213 CONSTRUCTION RECORDS

Complete construction records are available from the SCS office at the Broome County Airport. Several changes from the original design were made during construction. These changes have been indicated on the as built plans shown in Appendix E.

2.4 OPERATION RECORDS

Since the dam is an uncontrolled, floodwater retarding structure, no operating records are maintained regarding water levels. During periods of heavy rainfall, SCS personnel do monitor reservoir levels.

2.5 EVALUATION OF DATA

The data presented in this report has been compiled from information obtained

from the Soil Conservation Service as well as the New York State Department of Environmental Conservation files. It appears to be adequate and reliable for Phase I inspection purposes.

SECTION 3: VISUAL INSPECTION

principal spillway riser.

3.1 FINDINGS

<u>a. General</u>
<u>Visual inspection of the Site 2 Dam was conducted on November 8, 1979.</u>
The weather was overcast and the temperature was in the forties. The water surface at the time of the inspection was at the crest of the

b. Embankment
No signs of distress were observed in the earth embankment and no evidence of seepage, misalignment, subsidence, or surface cracking were noted on the embankment. Several minor deficiencies were noted. Vehicle wheel paths had been worn into the crest. A small bush was growing on the upstream slope at the east end of the dam. There was a depression on the upstream slope in the vicinity of the principal spillway riser. This depression might have been the result of scouring action of water flowing into the riser.

An internal drainage system composed of 2 - 10 inch diameter pipes surrounded by "drain fill" material and extending parallel to the axis of the dam provides drainage at the embankment-subgrade contact. These pipes outlet into the plunge pool adjacent to the principal spillway conduit. At the time of the inspection, each pipe was discharging a small quantity of clear water.

c. Principal Spillway
The principal spillway consists of a vertical drop inlet structure, a
cast-in-place rectangular concrete conduit, a plunge pool at the outlet
to the conduit, and an outlet channel. These components appeared to be in
satisfactory condition. The only deficiency noted was a build up of debris
surrounding the inlet to the spillway riser.

d. Auxiliary Spillway
The auxiliary spillway for this structure is located in an earth and rock
cut at the eastern end of the dam. The channel was in satisfactory
condition. However, there was a rather large area in which water ponds on
the channel bottom. In some places this water was as much as 6 inches deep.

e. Reservoir Drain
The 24 inch diameter reservoir drain and manually operated slide gate may be used to lower the reservoir. The slide gate control mechanism is located at the top of the riser. This system was reported to be operational.

f. <u>Downstream Channel</u>
The downstream channel below the plunge pool is riprapped. The channel appeared to be in satisfactory condition.

<u>q. Reservoir</u>
There were no signs of soil instability in the reservoir area.

3.2 EVALUATION

Visual inspection of this dam revealed the following deficiencies:

- 1. A small depression on the upstream slope behind the principal spillway riser.
- 2. Wheel paths worn into the embankment along the crest.
- 3. Debris collecting around the inlet to the principal spillway riser.
- 4. Ponding in the bottom of the auxiliary spillway channel.

SECTION 4: OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

The normal water surface elevation is at the crest elevation of the principal spillway riser. Downstream flows are limited by the flow over the principal spillway riser, except during periods of extremely heavy runoff when the auxiliary spillway is in service.

4.2 MAINTENANCE OF THE DAM

The dam is maintained by the owner, Broome County. Increased maintenance is required to correct deficiencies such as the debris surrounding the principal spillway riser and the water ponding in the auxiliary spillway channel.

4.3 WARNING SYSTEM IN EFFECT

There is no warning system in effect.

4.4 EVALUATION

The operation procedures for this structure are satisfactory. Increased maintenance efforts are required to correct the deficiencies noted above.

SECTION 5: HYDROLOGIC/HYDRAULIC

5.1 DRAINAGE AREA CHARACTERISTICS

Delineation of the 11.72 square mile watershed of the Site 2 dam was made using the USGS 7.5 minute quadrangle for Castle Creek, New York. The watershed consists of open grassed fields and woodlands. Relief in the drainage area ranges from moderate to steep.

The analysis for this report was performed using the entire drainage area for this structure. There are several other dams which are part of this watershed project upstream of this reservoir. No attentuation due to storage in these reservoirs was assumed in this analysis.

5.2 ANALYSIS CRITERIA

The analysis of the floodwater retarding capability of this dam was performed using the Corps of Engineers HEC-1 computer program. Dam Safety version. This program develops an inflow hydrograph using the "Snyder Synthetic Unit Hydrograph" method and then uses the "Modified Puls" flood routing procedure. The spillway design flood selected was the Probable Maximum Flood (PMF) in accordance with the Recommended Guidelines of the U.S. Army Corps of Engineers.

5.3 SPILLWAY CAPACITY

The principal and auxiliary spillways are ungated structures. The capacities for both spillways were taken from the stage-discharge curves included in the SCS design computations folder.

The spillways have sufficient capacity for discharging the peak outflow from the PMF. For this storm, the peak inflow is 12,746 cfs and the peak outflow is 12,657 cfs. When the spillways are discharging the peak outflow, the water surface will be 10.9 feet below the top of the dam. Further information concerning this analysis is included in Appendix C.

5.4 RESERVOIR CAPACITY

Normal flood control storage capacity of the reservoir between the principal and auxiliary spillway is 291 acre-feet which is equivalent to a runoff depth of 0.5 inches over the drainage area. Surcharge storage capacity to the maximum high water elevation is an additional 1180, acre-feet, equivalent to a runoff depth over the drainage area of 1.9 inches. Total storage capacity of the dam is 1480 acre-feet.

5.5 FLOODS OF RECORD

The maximum known flood occurred on September 27, 1975. The pool level at this time was reported to be about 5.0 feet above the principal spillway crest. The calculated discharge for this flood is as follows:

Elevation (USGS) Discharge (cfs) 787

5.6 OVERTOPPING POTENTIAL

Analysis indicates that the total discharge capacity is sufficient to prevent overtopping from the PMF.

5.7 EVALUATION

This dam has sufficient capability to impound and adequately discharge floodwaters expected to result from the PMF.

SECTION 6: STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

- a. <u>Visual Observations</u>
 No signs of distress were observed in connection with the earth embankment.
- b. Design and Construction Data
 No information regarding the slope stability analysis performed for the design of this structure was available from SCS. A slope stability analysis of the earth embankment is beyond the scope of work of this Phase I report. However, the slopes are relatively flat and there was no evidence of any instability.
- c. Seismic Stability No seismic stability analysis was performed for this structure.

SECTION 7: ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety
The Phase I inspection of the Finch Hollow Dam Site 2 dam did not reveal conditions which constitute a hazard to human life or property. The earth embankment is considered to be structurally stable and the spillways are capable of retarding and safely discharging floodwaters resulting from the Probable Maximum Flood (PMF).

b. Adequacy of Information Information reviewed for Phase I inspection purposes is considered to be adequate.

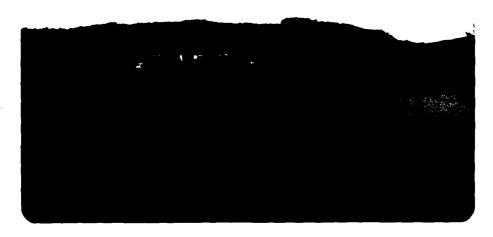
c. Need for Additional Investigations
No additional investigations are necessary at this time.

7.2 RECOMMENDED MEASURES

- a. Repair the small depression on the upstream slope behind the principal spillway riser.
- b. Modify the grading in the auxiliary spillway channel to eliminate the ponding.
- c. Remove the debris which surrounds the intake of the principal spillway riser. Provide a program of periodic inspection and maintenance of the dam and appurtenances, including operation and lubrication of the slide gate mechanism. Document this information for future reference.
- d. Develop an emergency action plan for notification of downstream residents and the proper authorities in the event of large auxiliary spillway discharge.

APPENDIX A

PHOTOGRAPHS



CREST of EMBANKMENT LOOKING WEST



OUTLET of PRINCIPAL SPILLWAY CONDUIT and DOWNSTREAM CHANNEL



UPSTREAM SLOPE of EMBANKMENT and PRINCIPAL SPILLWAY RISER

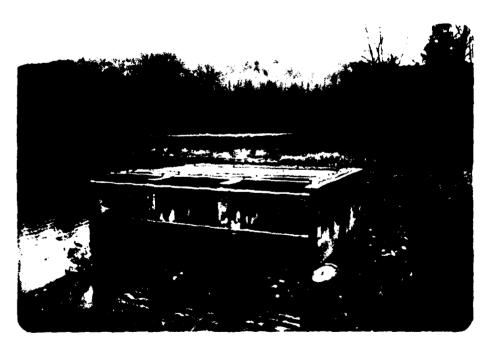


PHOTO SHOWING RELATIVE LOCATIONS of PRINCIPAL SPILLWAY RISER and ENTRANCE to AUXILIARY SPILLWAY CHANNEL



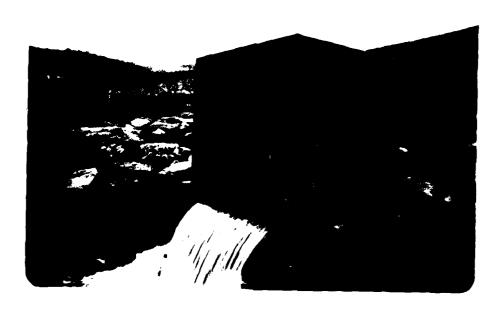
PRINCIPAL SPILLWAY RISER NOTE DEBRIS AROUND INLET



PRINCIPAL SPILLWAY RISER WITH INLET TO AUXILIARY SPILLWAY CHANNEL IN BACKGROUND



OUTLET to PRINCIPAL SPILLWAY CONDUIT



OUTLETS to PRINCIPAL SPILLWAY CONDUIT and to INTERNAL DRAINAGE SYSTEM



ENTRANCE to AUXILIARY SPILLWAY CHANNEL



AUXILIARY SPILLWAY CHANNEL LOOKING DOWNSTREAM



PONDED WATER on BOTTOM of AUXILIARY SPILLWAY CHANNEL



DOWNSTREAM SLOPE of DAM WITH OUTLET to AUXILIARY SPILLWAY CHANNEL at RIGHT

APPENDIX B VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1)	R	20	ic	n	2+	2
_,	, D	as	TC.	v	αL	<u>a</u>

a.	General
	Name of Dam FINCH HOLLOW SITE NO. 2
	Fed. I.D. # 719 DEC Dam No. 96A-3844
	River Basin SUSQUENANNA
	Location: Town DICKINSON County BROOME
	Stream Name LITTLE CHOCONUT CREEK
	Tributary of
	Latitude (N) 42° 8.2′ Longitude (W) 75° 56.5′
	Type of Dam <u>EARTH</u>
	Hazard Category
	Date(s) of Inspection 11/8/79
	Weather Conditions 40° OVERCAST
	Reservoir Level at Time of Inspection 68% BELOW TOP OF RISER
b.	Inspection Personnel R. WARRENDER W. LYNICK
c.	Persons Contacted (Including Address & Phone No.) GARY PAGE - SCS AREA OFFICE
	BROOME Co. AIRPORT 607-773-2751
	SCOTT SNOVER 315-423-5526 SCS-STRACUSE OFFICE
d.	History:
	Date Constructed 1972 Date(s) Reconstructed
	V
	Designer SCS
	Constructed By PORT CANNON CONTRUCTION CO. VESTAL, NEWYORK
	Owner BROOME COUNTY

a.	Char	racteristics
	(1)	Embankment Material EARTH AND ROCK FILL
	(2)	Cutoff Type EARTH
	(3)	Impervious Core None
	(4)	Internal Drainage System PERFORATED PIPE SURROUNGED BY DRAIN FILL
	(5)	Miscellaneous ALL SLOPES HAVE A SATISFACTORY VEGETATIVE
		COVER EXCEPT FOR SMALL ROCKFILL AREA JUST ABOUE OUTLET CONSUIT
b.	Cres	
υ.		Vertical Alignment SATISFACTORY
		Horizontal Alignment CURVILINEAR - SATISFACTORY- THERE WAS A SIGNIFICANT ALTERATION TO ORIGINAL DESIGN - SEE AS BUILT PLANS
	(3)	Surface Cracks None
	(4)	Miscellaneous VEHICLE WHEEL PATH ALONG CREST. CREST 15 HIGHER THAN COUNTY AIRPORT ROAD-4 LANE DIVIDED
c.	Upst	ream Slope
	(1)	Slope (Estimate) (V:H) 1 on 3
	(2)	Undesirable Growth or Debris, Animal Burrows 1 SMALL BUSH
		AT EAST END OF DAM
	(3)	Sloughing, Subsidence or Depressions NONE - SCIENT DEPRESSION ON SLOPE SIDE OF RISER
		•

2) Embankment

(5)	Surface Cracks or Movement at Toe None
)own	astream Slope
(1)	Slope (Estimate - V:H) ON 2.5
(2)	Undesirable Growth or Debris, Animal Burrows None CROWN VETCA
w	ITH GRASS- SATISFACTORY VEGETATIVE COVER
(3)	Sloughing, Subsidence or Depressions N_{QNE}
(4)	Surface Cracks or Movement at Toe None
(5)	Seepage None
	occpage NOND
(6)	External Drainage System (Ditches, Trenches; Blanket) ROCH LINES
	CHANNELS ALONG ABUTMENTS ON DOWNSTREAM SLOPE
(7)	Condition Around Outlet Structure NEAUL RIPRAP EXTENDING /
	DOWNSTREAM CHANNEL BANKS ON RIGHT SIDE-LEFT SIDE-ROCK
(8)	Seepage Beyond Toe NONE

		(1)	Erosion at Contact NoNE
		(2)	Seepage Along Contact NoNE
3)			System
	a.		ription of System 10" DIAMETER ASBESTOS CEMENT PIPE ANIMAL GUARNS AT OUTLET
	b.	Cond	ition of System <u>SATISFACTORY - FUNCTIONING</u>
	c.		harge from Drainage System <u>LESS THAN GAL, PER MIN. FROM</u> TH - DISCHARGE WAS CLEAR WATER
4)			ntation (Momumentation/Surveys, Observation Wells, Weirs, ters, Etc.)
			NONE

The second second

5)	Res	<u>ervoir</u>
	a.	Slopes RIGHT SIDE-EMBANKMENT OF COUNTY AIRPORT ROAD
		LEFT SIDE- HILLSIDE - NATURAL
	b.	Sedimentation None APPARENT
	c.	Unusual Conditions Which Affect Dam NoNE
6)	Are	a Downstream of Dam
	a.	Downstream Hazard (No. of Homes, Highways, etc.) RTE 17 - COUNTY
	A	IRPORT ROAD - HIGHLY RESIDENTIAL AREAS IN JOHNSON CITY
	b.	Seepage, Unusual Growth NonE
		,
	c.	Evidence of Movement Beyond Toe of Dam Move
	•	Condition of Downstream Channel SATISEACTORY
	d.	Condition of Downstream Channel SA(156ACTORY
7)	<u>Spi</u>	llway(s) (Including Discharge Conveyance Channel)
		SCS SINGLE STAGE VERTICAL RISER W/6'x7' CONCRETE
	<u></u>	ONDUIT & ROCH CUT AUXILIARY SPILLWAY
	a.	General RISER-LARGE DEBRIS AT ALL ENTRANCES - PLUS ON ALL
		WEIR CRESTS & INTERMIXED WITH SUBMERGED STEEL
		BARS
	b.	Condition of Service Spillway - EXCEPT FOR DEBRIS THE
		PRINCIPAL SPILLWAY IS IN SATISFACTORY CONDITION

The state of the state of

	STANDING WATER IN INVERT OF THE CHANNEL. AREA IS
	JUST UPSTREAM OF THE AXIS OF THE DAME DOWNSTREAM
	SPILLWAY OUTLET-NATURAL VERTICAL ROCK PLUNGE INTO DOWNS
l.	CHARNEL Condition of Discharge Conveyance Channel SATISFACTORY
?es	ervoir Drain/Outlet
(CO	Type: Pipe Conduit Other
	Material: Concrete Metal Other
	Size: 24" Length 46'
	Invert Elevations: Entrance 922,9 Exit 918,3
	Physical Condition (Describe): Unobservable /
	Material:
	Joints: Alignment
	Structural Integrity:
	Hydraulic Capability:
	Means of Control: Gate Valve Uncontrolled
	Operation: Operable Other

THE PARTY NAMED IN

Str	uctural
a.	Concrete Surfaces ALL SATISFACTORY
b.	Structural Cracking NONE APPARANT
c.	Movement - Horizontal & Vertical Alignment (Settlement) NovE
d.	Junctions with Abutments or Embankments
е.	Drains - Foundation, Joint, Face
f.	Water Passages, Conduits, Sluices SATISFACTORY
	·
g.	Seepage or Leakage Nane OBSERVED
	·

Foundation
Abutments
Control Gates
Approach & Outlet Channels
Energy Dissipators (Plunge Pool, etc.) NATURAL ROCK W/RINGS TO ELEVATION OF TOP CONSUIT
Intake Structures RISER OHAY EXCEPT FOR THE DEBRIS
Stability

APPENDIX C

HYDROLOGIC/HYDRAULIC ENGINEERING DATA AND COMPUTATIONS

CHECK LIST FOR DAMS HYDROLOGIC AND HYDRAULIC ENGINEERING DATA

AREA-CAPACITY DATA:

		Elevation (ft.)	Surface Area (acres)	Storage Capacity (acre-ft.)
1)	Top of Dam	976.4	69.0	1480
2)	Design High Water (Max. Design Pool)	958.8	41.7	590
3)	Auxiliary Spillway Crest	950,8	30,9	300
4)	Pool Level with Flashboards			
5)	Service Spillway Crest	931.6	4.7	20

DISCHARGES

	DISCHARGES	Volume (cfs)
1)	Average Daily	
2)	Spillway @ Maximum High Water	32,200
3)	Spillway @ Design High Water	5,270
4)	Spillway @ Auxiliary Spillway Crest Elevation	1,889
5)	Low Level Outlet	48
6)	Total (of all facilities) @ Maximum High Water	32,200
7)	Meximum Known Flood	787

CREST:		ELEVATION:	976,4
Type: GRASSED EARTH	·	·····	
Width:(4	Le	ngth: <u>1050</u>	····
Spillover AUXILIARY CHAP		·	
Location <u>EASTERN</u> END	OF DAM		
SPILLWAY:			
PRINCIPAL	•	EMERG	ENCY
931.6	_ Elevation _	950.8	
RC DROP INLET	Туре	TRAPE ZOIDA	L CHANNEL
6'X18'	_ Width .	751	
Тур	e of Control		
-		V	
	Controlled:		
	Туре		
(Flash	boards; gate)	
	Number		
	ize/Length		
Inve	ert Material		·····
Antic of ope	ipated Lengt	h ce	
C1	nute Length _	·	
Height Be & Appro	etween Spillw Dach Channel (Weir Flow)	ay Crest Invert	· · · · · · · · · · · · · · · · · · ·

Type: Gate Sluice	ė	Conduit	Penst	ock _	
Shape : GATE - FLAT CIRC	CULAR	CONDUIT	ROUND	CAST	/RON
Size: 24"		. ک	1!		
Elevations: Entrance Invert	922,9				;
Exit Invert	921.4				-
Tailrace Channel: Elevation					-
NADDONE ELDA OCTORE CACES	•				
HYDROMETEROLOGICAL GAGES:					
Type: NONE					
Location:					
Records:					
Date - NONE					
Max. Reading -					
FLOOD WATER CONTROL SYSTEM:	•	•			
Warning System: NonE					
	 				•
Method of Controlled Releases		:			
RESERVOIR DRAG	N				

AINAGE AREA: 11.72	.so.ml:
AINAGE BASIN RUNOFF CHARAG	CTERISTICS:
Land Use - Type: RES	LIDENTIAL + OPEN FIELDS
Terrain - Relief: Mot	
Surface - Soil: GLAC	
Runoff Potential (existi	ing or planned extensive alterations to existing ce or subsurface conditions)
NONE - BUT	TLAND IS DEVELOPABLE
Potential Sedimentation NonE	problem areas (natural or man-made; present or fut
Potential Backwater problems including surcharg	blem areas for levels at maximum storage capacity ge storage:
SEWAGE PUM	P STATION 6' BELOW UPSTREAM
	LEWIS ROAD - CONSTRUCTED AFTER
DAM WAS BUT	
	rflow & non-overflow) - Low reaches along the
Location: NonE	
Elevation:	
Reservoir:	•
Length @ Maximum P	Pool(Miles)
length of Shorelin	ne (A Snillway Crest) (Wilco)

PROJECT GRID

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LITTLE CHOCONUT CREEK WATERSHED SITE 2 NY-2015-D

DESIGN DATA

Site Location: Latitude 42 ⁰ 08'?	T MCM			INTO	OU A NOT ON!
Drainage Area:	ITEM			UNIT	QUANTITY
	Site Location:			••	42 ⁰ 081 28" 75 ⁰ 57! 321
Class of Structure: Principal Spillway: Pipe size (inside diameter) Riser size Pipe length (approx.) Riser Crest Elev. Pipe Outlet Invert Elev. Emergency Spillway: Bottom width Ft. Evel section length Ft. Entrance length Roughness coefficient Entrance slope (So) Entrance slope (So) Frich Entrance Spillway: Frich Entrance Stope (So) Frich Exit slope (Se) Frich	Drainage Area:			Acres	3,200
Pipe size (inside diameter) Ft. 6x7 Riser size Ft. 6x18 Pipe length (approx.) Ft. 310 Riser Crest Elev. Ft. 931.6 Pipe Outlet Invert Elev. Ft. 918.0 Emergency Spillway: Bottom width Ft. 75 Level section length Ft. 50 Entrance length Ft. 400 Roughness coefficient 0.04 Entrance slope (S_0) Percent 2 Crest elevation (E_0) Ft. 950.8 Exit slope (S_0) Percent 2.5 Storage: Retarding $(Min. V_{Sp})$ Ac.Ft. 300 Releases: Peak Principal Spillway (Q_p) cfs 1089 Emergency Spillway Hydrograph E_w Ft. 958.8	Class of Struct	ure:		•	(c)
Bottom width Ft. 75 Level section length Ft. 50 Entrance length Ft. 400 Roughness coefficient 0.04 Entrance slope (S_0) Percent 2 Crest elevation (E_e) Ft. 950.8 Exit slope (S_e) Percent 2.5 Storage: Retarding $(Min. V_{sp})$ Ac.Ft. 300 Releases: Peak Principal Spillway (Q_p) cfs 1089 Emergency Spillway Hydrograph E_w Ft. 958.8	Pipe size (in Riser size Pipe length (Riser Crest E Pipe Outlet In	side diamete approx.) lev. nvert Elev.	r)	Ft. Ft. Ft.	6x18 310 931.6
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Emergency Spillway Hydrograph E _w Ft. 958.8		al Spillway	(Q _p)	cfs	1089
Top of Dam Ft. 976.4	Emergency Spill	lway Hydrogra	aph E _w	Ft.	958.8
	Top of Dam			Ft.	976.4

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COMPUTATION SHEET

U. 5. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE

STATE

NEW YORK

PROJECT

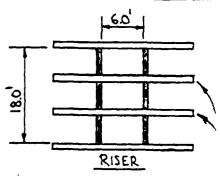
LITTLE CHOWNUT CREEK W.S.

SUBJECT

FLOW CONSTANTS FOR RISER & MONOLITH SHEET

. NY - 2015 - D

WEIR FLOW - CREST OF RISER



Q = CLH3/2

0 = (3.1)(350) H3/5

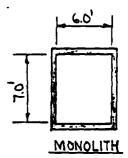
 $Q = 99.2 \, \text{H}^{3/2}$

NOTE: TWO SPLITTER WALLS 1.0 THICK WERE USED.

:. L= 18+18-4(1) = 32.0 ff

c = 3.1

PIPE FLOW - FOR 7x6 CONCRETE MONOLITH



Q=(0.597) (42.0) (8.02) h/2

Q= 201.09 h1/2

$$h = 0.013$$

(290)

$$K_c = 0.00260$$

C= 0.597

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NEW YORK STAFF DEPT OF ENVIRONMENTAL CONSERVATION FLUGO PROTECTION BUREAU **经验检验检验检验检验检验检验检验检验检验检验检验检验检验**

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UNIT HYDROGRAPH DATA 5.40 CP=0.63 111A= 0 1P=

STRTG= -2.00 ORCSN= -0.05 RTI:NE 1.00 APPADXIMATE CLANK CUEFFICIE ITS FRUM SIYDER CP AND TP ARE TC=11.98 AND R=10.05 INTERVALS RECESSION DATA

VDL. 1.60 133. 152. 167. 23. 5.39 MBPS, CPm 0.63 (55% 759 759 204 184 10. 26 10. 26 10. 9 225. 225. 83. 31. 60 END-OF-PERIOD ORDINATES, LAG. 185. 234. 413. 673. 249. 2743. 275. 101. 421. 303. 112. 41. UNIT HYDROGERAPH 335. 124. 124. 373.

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STATION 15 PLAN 15 RATIO 2

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PEAK FLOW AND STORAGE (END OF PERLIND) SUMMARY FORMULTIPLE PLAN-RATIO ECONDMIC COMPUTATIONS

		4	FLUAS	AREA 1'S SU	FLUMS IN CURIT FEET PER SECUND (CHITC METERS PER SECOND) AREA 1:3 SQUARE :41LES (SQUAR! KILOHFTERS) AREA 1:3 SQUARE :41LES (SQUAR! KILOHFTERS) ARTINS APPLIED TO FLOWS
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	~ `	11,72	~`	6242	12657

SUMMARY OF DAM SAFETY ANALYSIS

PLAN

	TIME OF FAILUME HOURS 0.
TUP UF DAM 976.40 1480.	TIME DF MAX DUTFLDW HDURS 45.50
	DURATION UVER TUP HOURS 0.
SFILLEAV CREST 931.60 9.	MAXIMUM UNTFLUM CFS 6242.
VALUE • 60 • 9.	MAXIMUN STURAGE AC-FT 647.
Ir ITIAL VALUE 931.60 9.	MAKIMUM UEFTH UV: 3 DAM O.
ELEVATION Storage Outflow	MAXIMUM RESEPUDIR W.S.ELEV 955.92
	RATIU OF 0.50

APPENDIX D REFERENCES

APPENDIX D

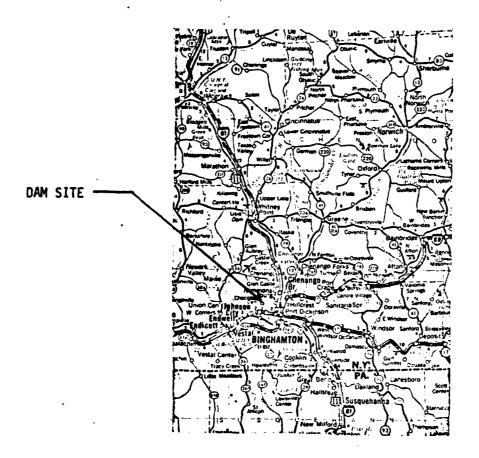
REFERENCES

- 1) U.S. Department of Commerce; Weather Bureau;

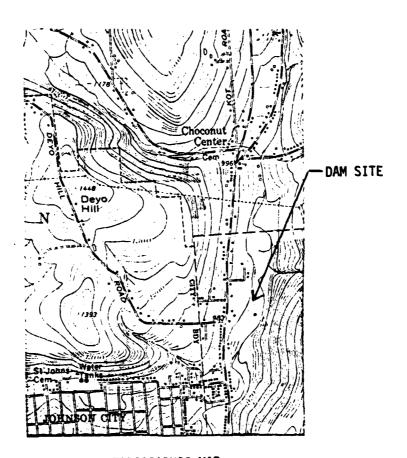
 Hydrometeorological Report No. 33 Seasonal Variation of the Probable

 Maximum Precipitation East of the 105th Meridian for Areas from 10 to
 1,000 Square Miles and Durations of 6, 12, 24, and 48 Hours, April 1956.
- 2) H.W. King and E.F. Brater, <u>Handbook of Hydraulics</u>, 5th edition, McGraw-Hill, 1963.
- 3) University of the State of New York, Geology of New York, Education Leaflet 20, Reprinted 1973.
- 4) Elwyn E. Seelye, Design, 3rd edition, John Wiley and Sons, Inc., 1960.
- 5) U.S. Department of the Interior, Bureau of Reclamations; Design of Small Dams, 2nd edition (rev. reprint), 1977.

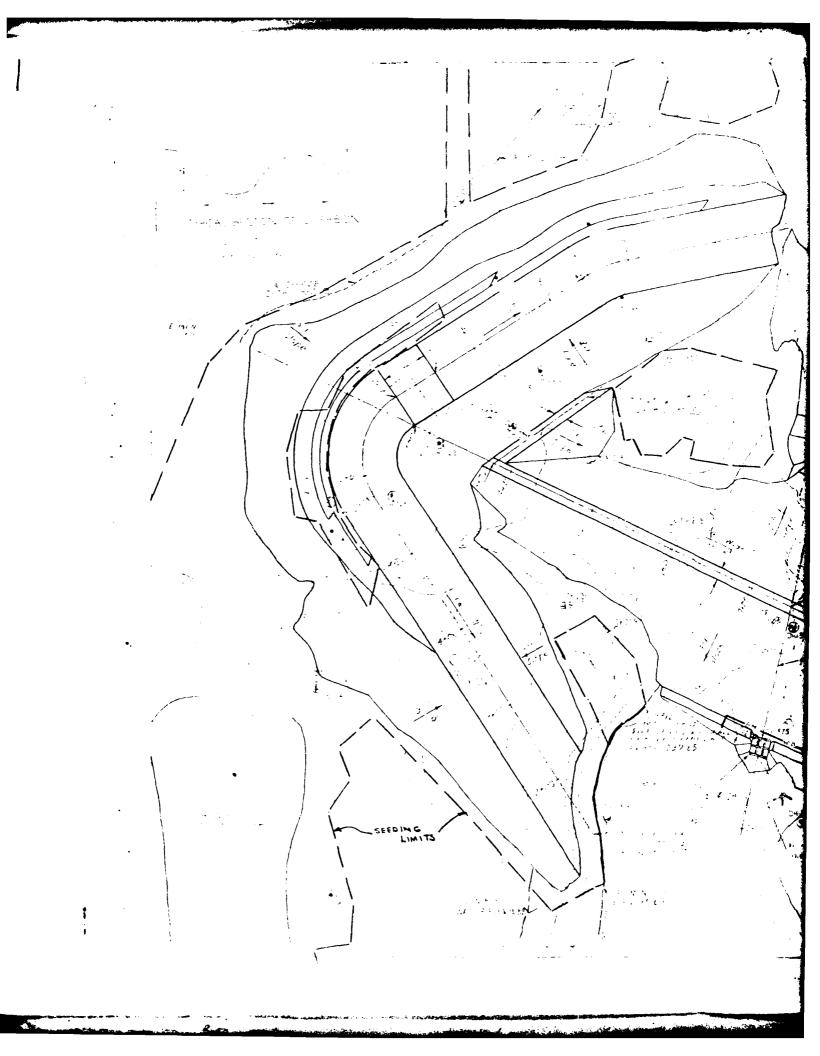
APPENDIX E DRAWINGS

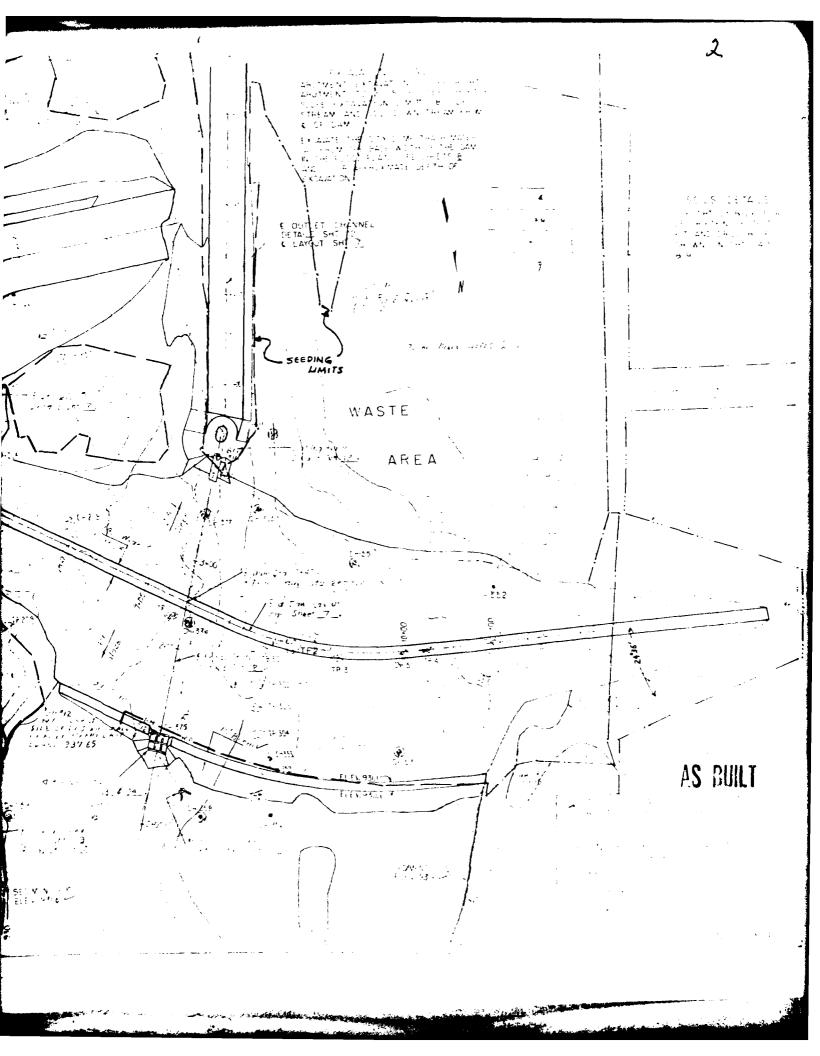


VICINITY MAP
FINCH HOLLOW WATERSHED PROJECT
SITE 2
I.D. No. NY 719



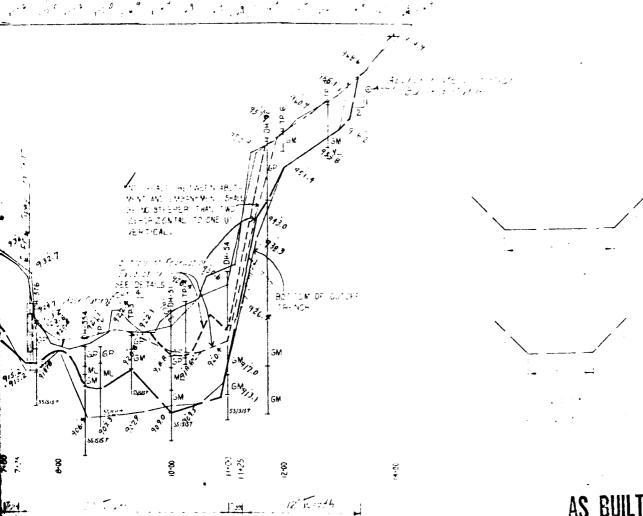
TOPOGRAPHIC MAP
FINCH HOLLOW WATERSHED PROJECT
SITE 2
I.D. No. NY 719





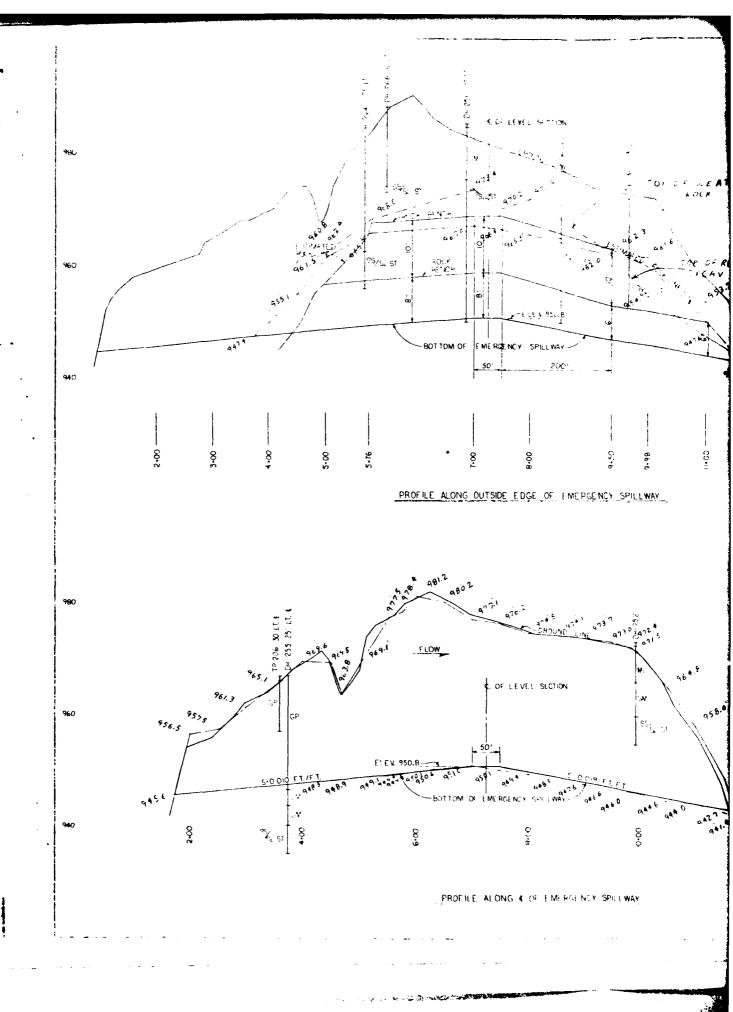
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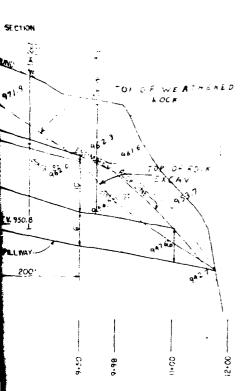
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FINAL HOLLOW, EITTLE CHOOMIT 8 THOUT BHOOK WATERSHED PROJECT WATER HITCHING DAM NO 2 THE HITCHING HEEK

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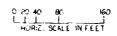


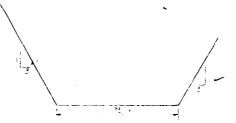
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OF EMERGENCY SPILLWAY

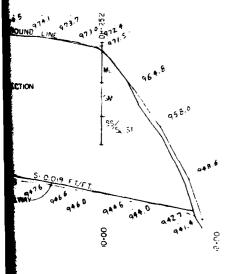


ROCK EXCAV 27551 CU. JUS.





SECTION OF EVERGENCY SPELWAY AT STATULISHOD, TYPICAL FROM AFFORESTMON HIGH TO CHSTALAM INTERSECT UP CHROCK EXCAPATION AND FROM LIMITORISM INTERSECT IN THIS E EXCAPATION TO APPROXISTATION (HBC

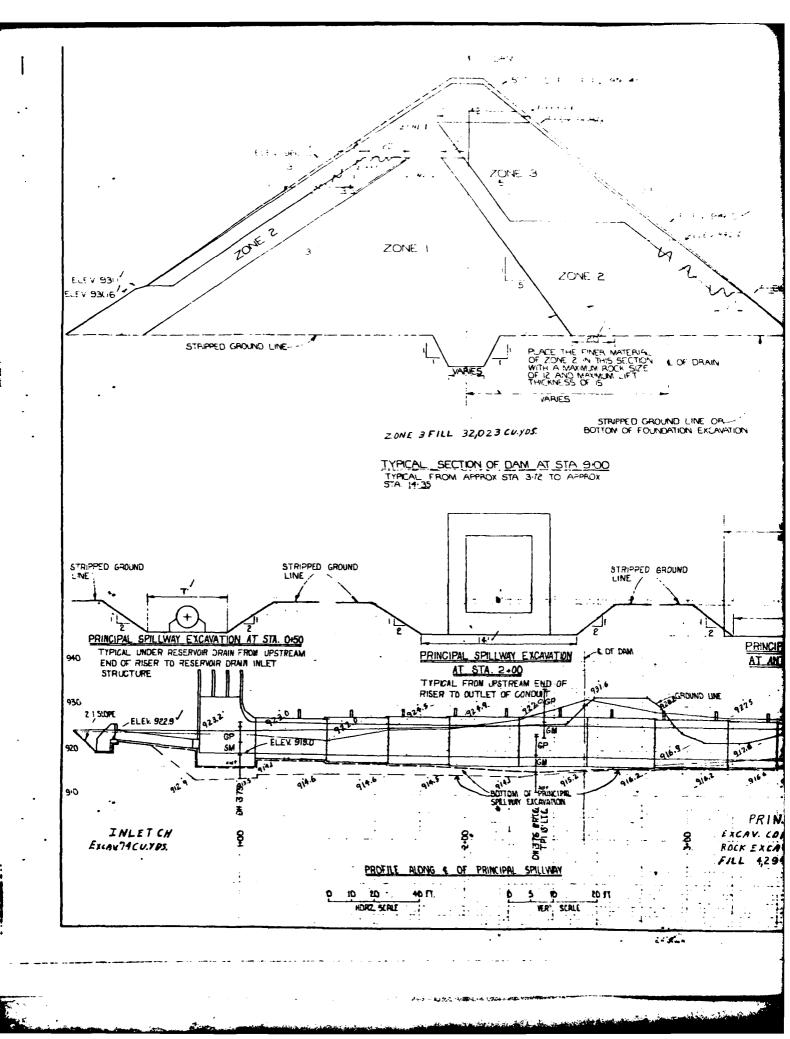


MERGENCY SPILLWAY

AS BUILT

FINCH HOLLOW, LITTLE CHOCONUT & TROUT BROOK WATER HED FROJECT FLOW WATER HETAE AND WILL THE CHOCON, THEFE EMERGENCY OPILEWAY

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2016	MATERIAL 1/	ROOK	HAX. HEIFT TIMICA	MIN. REGITRED		COMPACTION E
L] ≛		HATER CONTENT	CLASS	DEFINITION
1	REPRESENTED BY MATERIAL IN TEST PIT 103 (0.5 11.0) TEST PIT 108 (0.5 -11.0) TEST PIT 108 (0.5 -11.0) TEST PIT 203 (1.7 -4.0) DRILL HOLE 252 (7.1 -13.2)	,		PERCENTAGE POINTS RELOW OPTINGM	•	Fig. 68 SAXIMIN DESCITS BY ASTR D=094 M21H0D C
?	OVERSIZE MATERIAL REMOVED FROM ZONE 1 AND QUBBLES, GRAVEL, SAND, SILT AND RECCIATED HEDROCK REPRESENTED BY TEST PIT 3 (3 01-6.5') TEST PIT 205 (1.5-17.0') DRILL HOLE 252 (2.6'-13.2')	24-	36"	2'		SEE CONSTRUCTION 5
1	ROCK FROM THE EMERGENCY SPILLWAY	14"	74*		×	SEE CONSTRUCTION SPECIFICATION 5

1/ THE PLACEMENT TABLE INDICATES ESTIMATED USE OF MATERIAL.

1/A. MAXIMUM ROCK SIZE PLACED IN BACKFILL COMPACTED BY MEANS OF HAND TAMPING ON MANUALLY DIRECTED POWER TAMPERS ON PLATE VIBRATORS SMALL BE 3".

5. DOVERSIZE MATERIAL (6"-24") TO BE GRADED WITHIN ZONE 2, SC THAT THE LARGER RICKS ARE PLACED TOWARD THE DOWNSTREAM SLOPE.

IUMAND THE DUMNSTMEAM SLUPE.

/ HAXIMUM LIFT THICKNESS PRIOR TO COMPACTION.

/ WATER CONTENT AT TIME OF COMPACTION.

/ THOROUGHLY WET BUT:

ANOTHORE THAN 12T MOISTURE CONTENT BASED ON THE MINUS 3/4" SIEVE UNLESS MODIFIED BY THE ENGINEER
AT THE TIME OF CONSTRUCTION.

b. NOT SO WET AS TO CAUSE ADHERENCE OF THE SOIL TO THE WHEELS OR TRACKS OF EQUIPMENT, NOR TO CAUSE MOGGING DOWN OF EQUIPMENT.

FOR TYPICAL COMPACTION CURVES SEE THIS SHEET.

CONSTRUCTION DETAILS

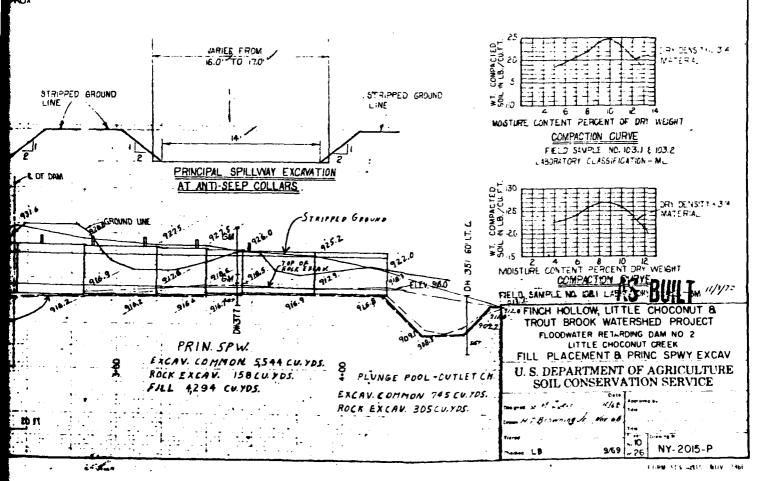
- THE FOUNDATION SURFACE THROUGHOUT THE BASE AREA OF THE DAM SHALL BE SCARIFIED (EXCEPT WHERE POUNDATION IS BEDROCK) TO A DEPTH OF ST AND COMPACTED PRIOR TO PLACEMENT OF EARTH FILL. SOME BOUNDARIES INDICATED ARE APPROXIMATE. ADJUSTMENTS WILL BE MADE BY THE ENGINEER TO PERMIT THE CONTRACTOR TO UTILIZE ALL USEABLE REQUIRED EXCAVATION WITHIN THE MEAT LINES OF
- THE EMBACEMENT.
 TOPSOIL THAT IS SUITABLE FOR USE SHALL BE INCORPORATED WITHIN THE SLOPES OF THE EARTH
 FILL AS DIRECTED BY THE ENGINEER.

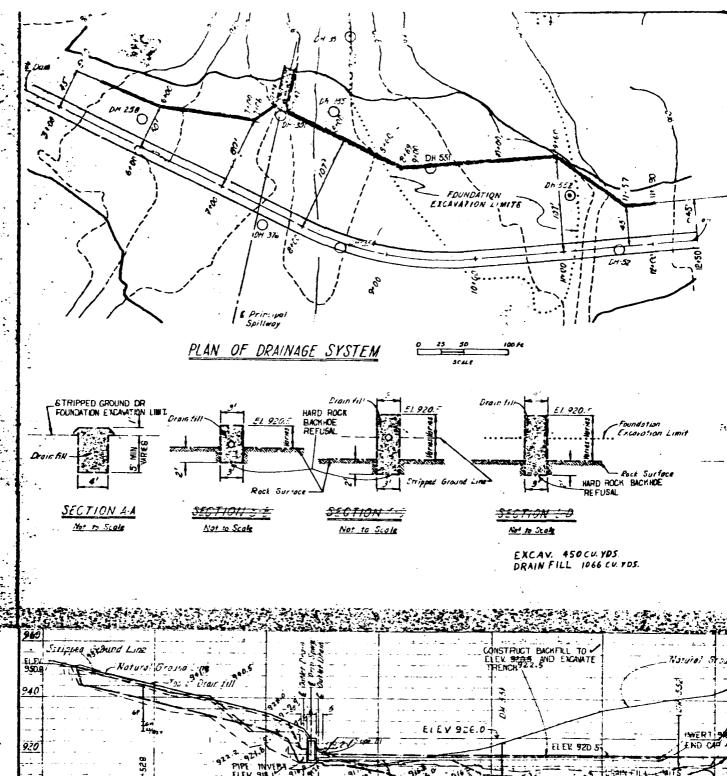
STRIPPED GROUND LINE OR-

L OF DRAIN

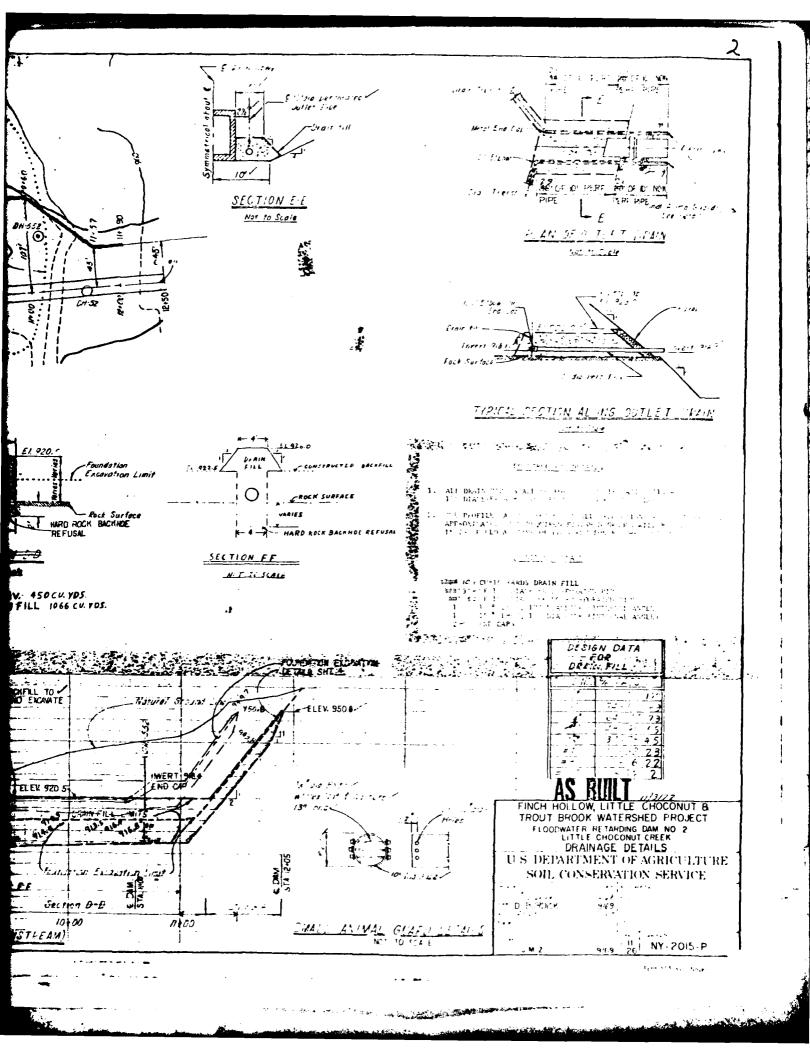
FINER MATERIAL IN THIS SECTION IN ROCK SIZE AXMON LIFT

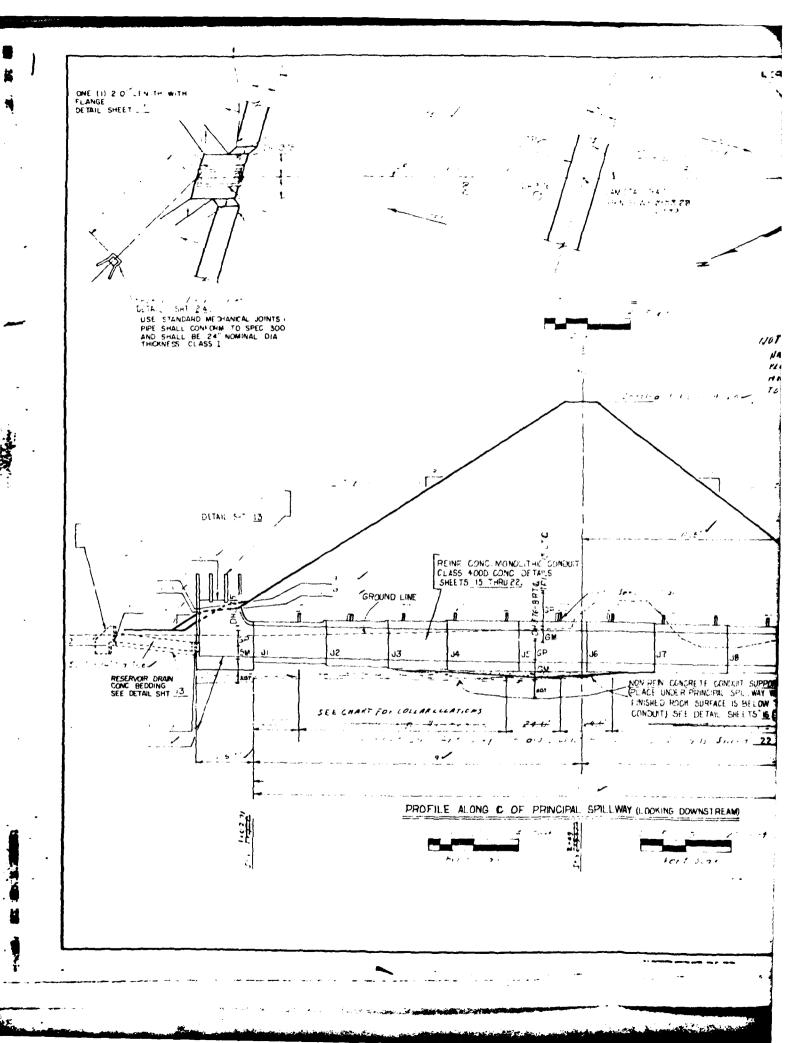
<u>9∙∞</u>

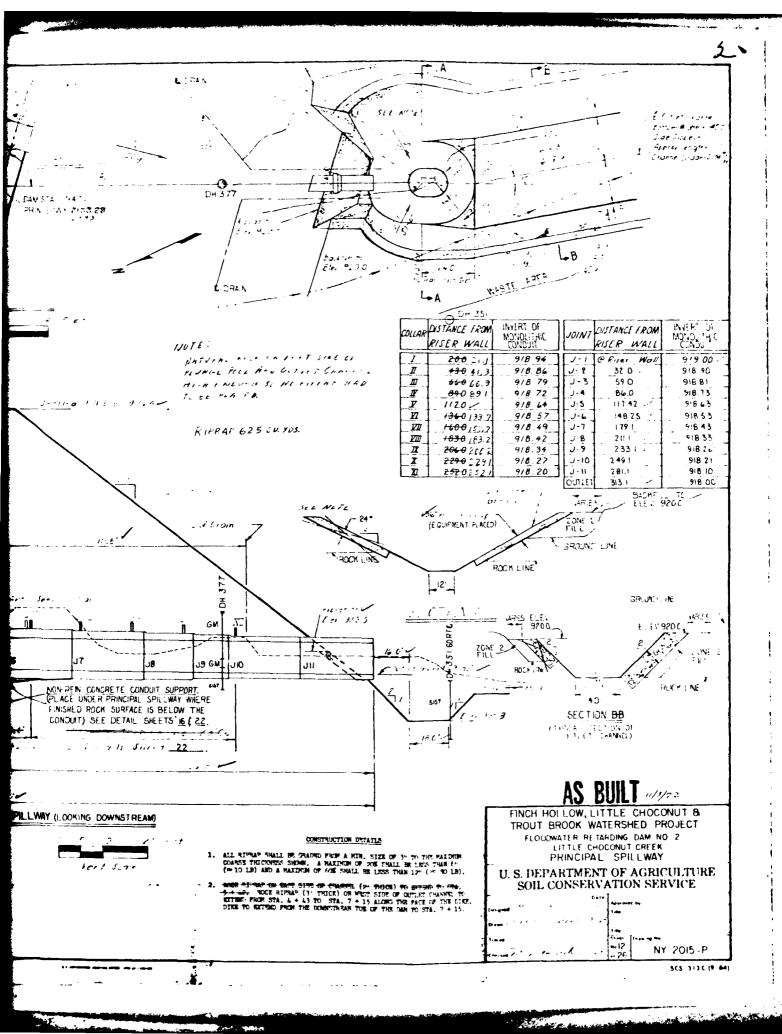


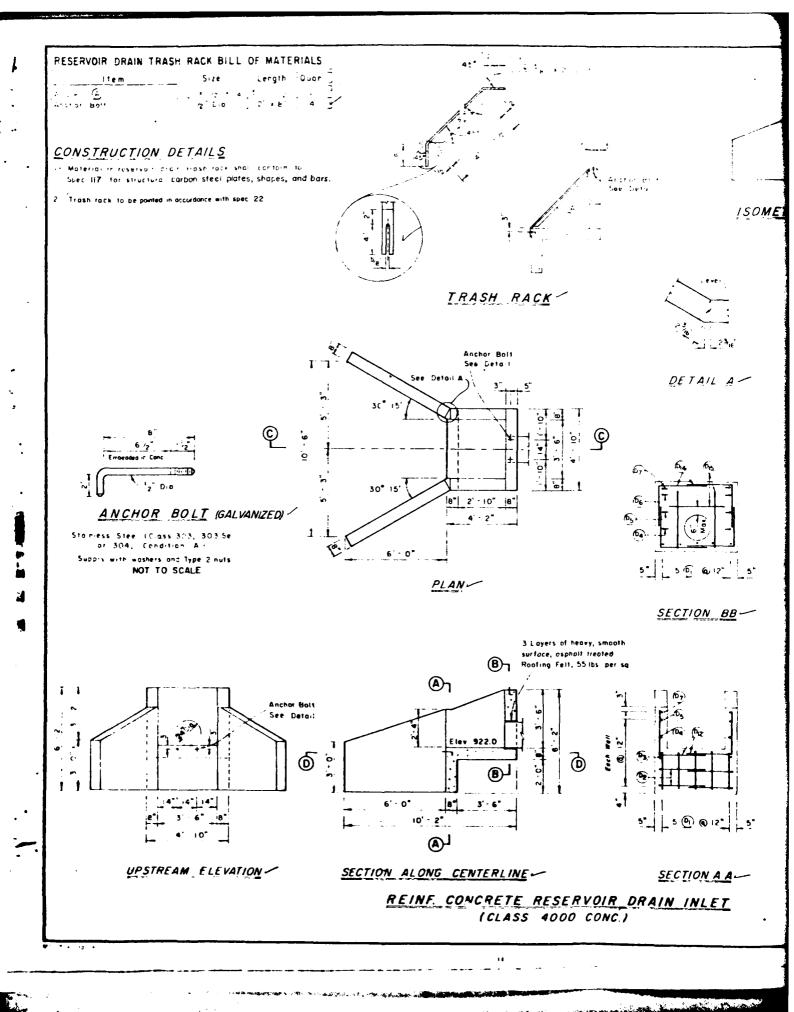


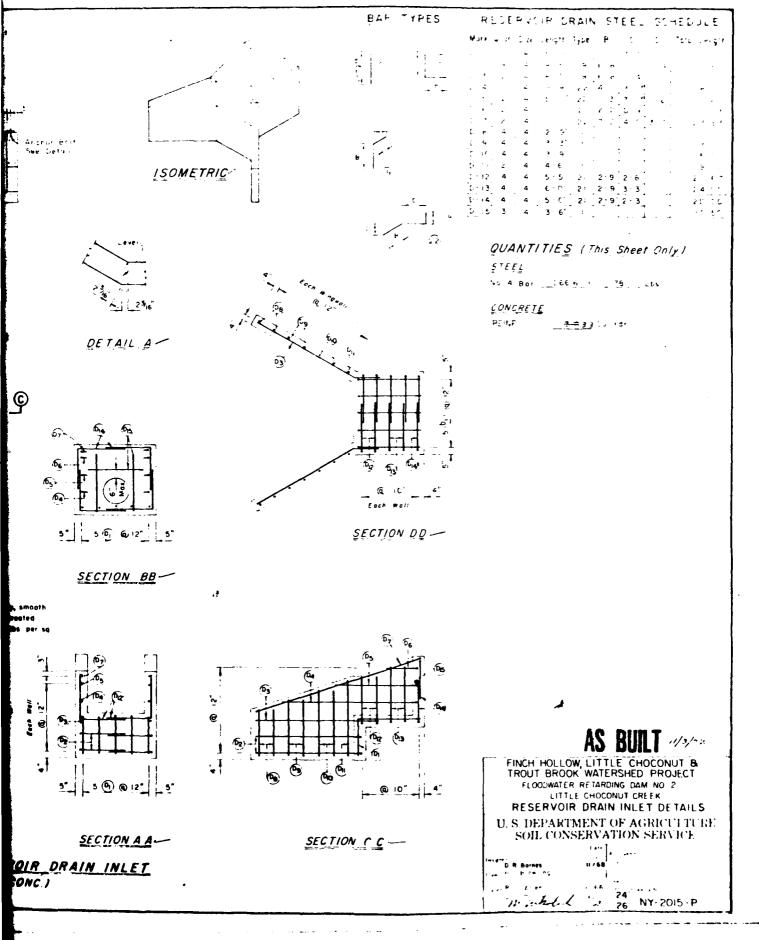
HORZ SCALE IN FEET SECTION FF Section B-B 7+00 5 00 9:00 10:00 CENTERLINE OF DRAIN TI OF MINE DOWNS THEAM!











MATERIAL DESCRIPTIONS

- -

A

Gravel, coarse - 375-70% angular to subangular combles and flagstume from 5" to 3t" size in silty matrix - yellow/brown - dry to moist - luose to paoked - repidity permeable - glactal till - Miscousin stage. (C

Gravel, coarse to medium - subangular and sub-rounded cobbles from 2"-5" dis., - some fines -brown, moist to wet - love to medium dense -rapidly permeable - recent alluvium. (GP (GP)

Gravel, silty - 20".-40". engular, often thin, weathered flagstones from 3"-12" size in silty matrix - large 3'-4' boulders common - brown - moist - dense - slowly permeable - glacial till - Wisconsin stage. (CM)

D

Bracciated shales - broken gray siltstone in silty matrix - slate gray - moist - slowly permeable - glacial moraine debria. (GM)

Sand, silty - 107-202 angular to subangular flagstones 3"-10" size - with gray silty lenses - brown - moiat - soft - medium permeable - glacial till - Wisconsin stage. (SM)

Silt, sandy - WOX smeller than #60 screen, some subengular flags - brown - moist - soft - medium permeable - ice contact deposit. (ML)

Silt, fine to coarse - no large aggregates - slate gray - moist - soft - slowly permeable - lacustrine deposit. (PL)

Siltatone, interbedded with fine grained, gray sandstone, sometimes varved, sound - hard - dense - fossilferous - horizontal bedding beds from thin to 16" - occasionally vertical tension finaures. (ss. slst)

City dump trash - 50% rubber refuse from local shoe industry - bouncing - smelling - moist to wet.

Topsoil - organic matter - some stones and boulders - brown - dry - loose - permeable.

BACKHOE PIT LOGS

TP 1..C/L. Elev. 934.4. . .

0 0.5 Topsoil - Material K 0.5 8.0 Material A (GP) 8.0 11.5 C (CH)

Ti 2, C/L, Elev. 919.4

0 3.0 Material E (G1) 3.0 7.5 F G (ML) D.S. 2.1 to 51 7.51 R (es, slst)

T) 3, C/L, Elev. 922.1

0 0.5 Topsoil - Material K 0.5 3.0 Material E (GP) 3.0 6.5 " D (GM) 6.5+ " H (ss, slst)

MOTE: Slight scepage (5.51.

17 4, C/L, Elev. 927.6

0 10.0 Material 1 10.0 11.0 " B (CP)

TI 5, C/L, Eler. 931.0

0 5.5 Material I 5.5 11.0 E E (291)

TP 6, C/L, Elev. 958.2

0.5 Topooil - Material F 4.0 Material C (GM)

Note: Note abandoned 441 due to heavy boulders.

TF 7, C/L, Elev. 964.3

0 1.0 Topaoil - Material K 1.0 7.0 Material E (SM) 7.0 9.0 " C (GM) 9.0 11.5 " G (ML) 1.0

Note: Slight septic tank effluent flow (46%. Small spring (418.5%.

TF 8, C/L, Elev. 962.9

0 0.5 Topsoil ~ Material K 0.5 8.0 Material C (SM) 8.0 10.0 " C (ML)

Note: Slight septic tank effluent flow (45.51.

Ti 101, Borrow Area, Elev. 995.2

0 0.5 Topsoil - Material F 0.5 11.0 Material E (SM)

TF 102, Borrow Area, Elev. 957.4

0 0.5 Topsoil - Heterial K 0.5 11.0 Material A (GP)

TP 103, BOTTOW Area, Elev. 978.4

0 0.5 Topsoil - Naterial K 0.5 11.0 Material E (SM) D.S. 103.1 06.51. D.S. 103.2 011.

TF 104, Sorrow Area, Elev. 1017.2

0 0.5 Topsoil - Material E 0.5 11.5 Material E (SM)

TP 105, Borrow Area, Elev. 992.7

0 0.5 Topsoil - Material K 0.5 9.0 Material E (SM) 9.0 11.0 " C (GM)

TF 106, Porrow Area, Elev. 976.9

0.5 Topmoil - Material K 9.0 Material C (CM) 9.0 11.5 " E (SM)

Note: Heavy boulders (shale) in Material C.

TP 107, Forrow Area, Elev. 990.9

0 0.5 Topsoil - Material K C.S 11.5 Material E (SM)

Ti 108, Forrow Free, Elev. 1007.3

0 0.3 Topsoil - Material F 0.3 10.5 Material C (CM) D.S. 108.1 (48).

Tr 109, Porrow Area, Elev. 964.1

0 0.5 Topsoil - Material K 0.5 3.0 Material C (CM) 3.0 8.0 " E (SM) 8.0 11.5 " A (G)

Tr 201, Emer. Spill., Flev. 959.8

1.5 Topsoil - Material K 8.0 Material A (GM)

1) 202, Fmer. Spill., Flev. 973.9

1.0 Topsoil - Material K 7.0 Material C (CM)

Ti 203, Emer. Spill., Elev. 965.2

0 1.5 Topsoll - Material F 1.5 5.0 Material E (SM) 5.0 10.0 " C (ML) 10.0 11.0 " D (GM) 10.0

71 204, Emer. Spill., Flev. 956.8

1.5 Topeol1 - Material k 9.0 interial C (GH)

77 205, Fmer. Spill., Elev. 958.4

D 1.0 7opsol1 ~ Material K 1.0 10.0 Material A (CH) D.S 2051

T. 21. tmer. Spill., Elev. 96: 0

0 1.0 Topactl - Material 1.0 10.0 Material A (GP)

TF 207, haer. Spill., blev. 983.6

0 1.0 Topsoil - Material 1.0 10.0 Material A (GF)

71 208, Emer. Spill., Flev. 982.0

0 3.0 Material C (QM) 3.0 7.0 T E (SM) 7.0 T H (ma, mle

TF 209, Fmer. Spill., Flev. 950.8

0 0.5 Topsoil - Material 0.5 9.6 Material A (GF) 9.0 11.5 F (ML) D.

Ti 216, Emer. Spill., Flev. 953.6

0.5 Topsoil - Material 7.0 Material A (G1) 9.0 " E (SM) 0.5

Note: Occasionally heavy bouldes

TF 301, Frin. Spill., Elev. 919.4

0 1.0 Material E (GF)
1.0 6.0 " D (GM)
6.0 " N (ss, sla

Ti 302, Frin. Spill., Llev. 919.7

0 3.0 Material 5 (Gi) 3.0 6.0 " C (ML) Maferiai n (oi) " C (NL) " H (ss. sl

Ii 303, Irin. Spill., Flev. 919.5

0 3.0 Material B (GP) 3.0 7.0 ° C (ML) 7.0+ " H (ss. al 3.0 7.0+

TF 304, Frin. Spill., Elev. 919.3

2.0 Material B (GP) 2.0 5.5 ° C (ML) D.S. 304.1 '6' MAT'L 5.5 10.5 Material D (CM)

hote: Medium seepage from adjag creek ::21.

Ti 305, Trin. Spill., Elev. 919.2

0 3.0 Material F (GF) 3.0 8.0 " D (GM)

DETLE HOLF LOCS

Dr. 51, C/L, Elev. 925.9

Material H

---0.0 Material 1 RB ---- A.O---KB ML. 40 -- 18,6-

23.0 DH 52, C/L Flev. 956.6

1 0.0. 1 0.0 Materi ____11.0__ R.A Haterial C __49.0__

Note: Hole abundaned due t

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[m.64 fm 3, m. 1.41 945 Em 5 Burres Arer e es 10.7 Silvarone Tricilladad wenttered tron 20 to 1000 Her 25 to 100 to .20**%** ! LH TE HOME 4 PC C 44 991 10 CO 10 Spay 1 20 5 70 Certuitaer Colum Indige Promitrown to grey Sauce E se form H 20 Sr no telore 20 st s at S. fater e - weathgred * * * *! -- 37 c ··· Im the Emilian Steel Feet 88 - : E Solidate that the second of th DH 53, Borrow Arec Elev 977 Auger Statere sound assist Overburden Color change from brown to grey at 25 N<u>ute</u> Exploratory hale for bedrock elev DH 267, Em Spwy - Eres 978 Si fatone - fractured O C Auger - 35 0 --- ---Thin tedded, loose from 13 = 48. Sound, 6° teds. 93 % OH 260, Err Spay - Eley 972 NX . - - 0 0 - 10 0 . - - - - - - Sitstone sound S Hatone ____ .
(2" 5" bedding from (4"-19) ___ sa = sist Fig. 1. Let A. Apple 1984 Dri 356 , Princ Spwy - Elev 922 -- 195 Places of the same regions for a fit stands on the region of the region 1826) Em 1289 Elev 975 .00.-· 6 in the state of the control of the c Overcurden - 25 0 -- 16 0 --Malerial D Auger | Sittstone. Thir bedded, weathered Dre marries was yeer Bother can to actual on site in same - 20 0 from 25 - 28 Sound, 2" - 6" hedding from 25" - 33 ss-8ist en cer cut to aloa de cute.

17.0 Lagre a oue fo.

18. El o core, las Michaeles.

18. El ocore end cure la versional months.

18. Corpora en ball.

18. Corpora en ball.

24.0 Sittstone - sound - ss/sist 100% DH 357, Princ Sowy - Elev 922 T wi late! mater level DH 262 , Em Spay - Elev 972 Suistone se/sist hote Exploratory hale for bedrack elev GEOLOGY NOTE DH 358 Princ Spwy - Elev 922 Siltstone Sound from (3.5"- (8.5" (RILL HOLES 151, 152, 153, 160, 261, 262, Material B 263, 264, 265, 266, AND 267 WERE INVESTI Thin bedded ordicloy seams from 18 5 - 21 5 Sound from 215'- 23 5' ss = sist MX SATED FOR DATA ON THE ELEVATIONS AND PHYSICAL CONDITION OF THE BELFIOCK AND Moterial D DO NOT INDICATE THE DETAILED DESCRIPTION OF THE OVERBURDEN Silfstone & 85/5/51 FINCH HOLLOW LITTLE CHOCONST & 100% | IB C -DH 263, EM SUMY - EVEN 970 Overburgen --DH 552, Drain Line | Elev 935 THOUT BROOK WATERSHED PROJECT City Cump Material 1 FIGURE CHOCONUT SREEK 5- Island 1 Thin bedded - '/a" bads -LUGS OF TEST HOLES wedthered fractured as/stat U.S. DEPARTMENT OF AGRICULTURE 40 SOIL CONSERVATION SERVICE - 25 0 - - - - -Sittatona - medinerad - ss fa at - 1.201 NY MB-PE We have been a supplied to the supplied to the